PCT.

WORLD INTELLECTUAL PROPERTY ORGANIZATION International Bureau



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 6: H04L 5/06, 27/26

A2

(11) International Publication Number:

WO 98/39872

(43) International Publication Date: 11 September 1998 (11.09.98)

(21) International Application Number:

PCT/SE98/00353

(22) International Filing Date:

27 February 1998 (27.02.98)

(30) Priority Data:

9700784-3 9703629-7

3 March 1997 (03.03.97)

6 October 1997 (06.10.97)

SE SE

(71) Applicant (for all designated States except US): TELIA AB (publ) [SE/SE]; Mårbackagatan 11, S-123 86 Farsta (SE).

(72) Inventors; and

(75) Inventors/Applicants (for US only): OLSSON, Lennart [SE/SE]; Majvägen 39, S-973 31 Luleå (SE). BAHLEN-BERG, Gunnar [SE/SE]; Blidvägen 234, S-976 32 Luleå (SE). BENGTSSON, Daniel [SE/SE]; Forskarvägen 36 A, S-977 53 Lulea (SE). HAKANSSON, Siwert [SE/SE]; Aprilvägen 10, S-177 61 Järfälla (SE). ISAKSSON, Anders [SE/SE]; Elevvägen 1, S-977 25 Luleå (SE). ISAKSSON, Lars-Åke [SE/SE]; Residensgatan 6 C, S-972 36 Lulea (SE). ISAKSSON, Mikael [SE/SE]; Borgmästarevägen 7, S-973 42 Lulea (SE). JOHANSSON, Magnus [SE/SE]; Timmermansgatan 34, S-972 41 Luleå (SE). LAHTI, Mauritz [SE/SE]; Lingonstigen 63, 3tr, S-973 33 Luleå (SE). LJUNGGREN, Lis-Marie [SE/SE]; Praktikantvägen 31, S-977 53 Luleå (SE). LUNDBERG, Hans [SE/SE]; Västra Solgatan 8, S-972 53 Luleå (SE). NORDSTRÖM, Tomas [SE/SE]; Docentvägen 279, S-955 52 Luleå (SE). OLOFSSON, Sven-Rune [SE/SE]; Malmuddsvägen 9, S-972 45 Luleå (SE). STEFANSSON, Tomas [SE/SE]; Lulavan 773, S-961 93 Boden (SE). ÖMAN, Hans [SE/SE]; Fältspatstigen 21, S-977 53 Luleå (SE). ÖKVIST, Göran [SE/SE]; Hagaplan 7, S-974 41 Luleå (SE).

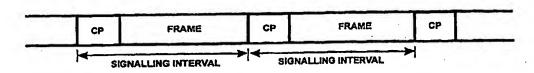
(74) Agent: PRAGSTEN, Rolf; Telia Research AB, Vitsandsgatan 9, S-123 86 Farsta (SE).

(81) Designated States: EE, LT, LV, NO, US, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).

Published

Without international search report and to be republished upon receipt of that report.

(54) Title: IMPROVEMENTS IN, OR RELATING TO SYNCHRONISATION



CP = CYCLIC PREFIX

(57) Abstract

With OFDM systems the frequency domain data is the Fourier transform of the received time domain OFDM frames. The time domain frames must be sampled, at the receiver, in synchronism with the transmitter, so that each received frame contains data from only a single transmitted frame. It is vital for this synchronism to be maintained in order to maintain the orthogonality of the frames. A typical multi-carrier system, of the OFDM type, which uses a cyclic prefix permits orthogonality to be maintained when there is a small deviation from exact frame synchronisation. Because the signalling interval includes both an entire frame and the cyclic prefix, which is a repetition of part of the frame, a frame sampled within the signalling interval will contain data from only one frame. Since the signalling interval is greater than the frame period, this gives some leeway in frame alignment. In a multi-carrier system of the OFDM type, an adaptive channel equalizer, operating in the frequency domain, is often used. The internal parameters in such an equalizer contain, in addition to information about the characteristics of the channel, information which can be interpreted as the time deviation between the sampling clocks of the transmitter and the receiver. The present invention utilizes this information to control the sampling clock of the receiver in a more robust way than has previously been possible with known techniques. The present invention is particularly suitable for use in ADSL and VDSL modems which can be used to give broadband access over copper networks. The invention is also of relevance to broadband transmission in mobile and semi-mobile systems for transmission over the radio channels.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Amenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav	TM	Turkmenistan
BF	Burkina Faso	GR	Greece		Republic of Macedonia	TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
		IS	Iceland	MW	Malawi	US	United States of America
BY	Belarus	IT		MX	Mexico	UZ	Uzbekistan
CA	Canada		Italy	NE	Niger	VN	Viet Nam
CF	Central African Republic	JP	Japan	NL	Netherlands	YU	Yugoslavia
CG	Congo	KE	Kenya	NO		zw	Zimbabwe
CH	Switzerland	KG	Kyrgyzstan		Norway	211	23modowe
CI	Côte d'Ivoire	KP	Democratic People's	NZ	New Zealand		
CM	Cameroon		Republic of Korea	PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakstan	RO	Romania		
cz ·	Czech Republic	LC	Saint Lucia	RU	Russian Pederation		
DB	Germany	LI	Liechtenstein	SD	Sudan		•
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		

WO 98/39872 PCT/SE98/00353

IMPROVEMENTS IN, OR RELATING TO SYNCHRONISATION

The present invention relates to an OFDM transmission system, an OFDM receiver, OFDM modems including ADSL modems and VDSL modems, and methods of synchronising an OFDM receiver with an incoming multi-carrier signal, in particular, the present invention relates to sampling clock oscillator control for an OFDM system.

In this specification the term OFDM (Orthogonal Frequency Division Multiplex) type is intended to include DMT (Discrete Multi-Tone).

The demand for provision of multi-media and other broad bandwidth services over telecommunications networks has created a need to transmit high bit rate traffic over copper pairs. This requirement has led to the development of a number of different transmission schemes, such as, ADSL (Asynchronous Digital Subscriber Line) and VDSL (Very high bit-rate Digital Subscriber Lines). One of the more likely modulation systems for all these transmission schemes is a line code known as DMT (discrete multi-tone), which bears a strong resemblance to orthogonal frequency division multiplex, and is a spread spectrum transmission technique.

In discrete multi-tone transmission, the available bandwidth is divided into a plurality of sub-channels each with a small bandwidth, 4kHz perhaps. Traffic is allocated to the different sub-channels in dependence on noise power and transmission loss in each sub-channel. Each channel carries multi-level pulses capable of representing up to 11 data bits. Poor quality channels carry fewer bits, or may be completely shut down.

Because inter pair interference in copper pair cables is higher where data is transmitted in both directions, i.e. symmetric duplex, a number of transmission schemes have proposed the use of asymmetric schemes in which high data rates are transmitted in one direction only. Such schemes meet many of the demands for high bandwidth services, such as, video-on-demand.

10

5

15

っ

VDSL technology resembles ADSL to a large degree, although ADSL must cater for much larger dynamic ranges and is considerably more complex as a result. VDSL is lower in cost and lower in power, and premises VDSL units need to implement a physical layer media access control for multiplexing upstream data.

Four line codes have been proposed for VDSL:

- CAP; Carrierless AM/PM, a version of suppressed carrier QAM, for passive NT configurations, CAP would use QPSK upstream and a type of TDMA for multiplexing (although CAP does not preclude an FDM approach to upstream multiplexing);
- DMT; Discrete Multi-Tone, a multi-carrier system using Discrete Fourier Transforms to create and demodulate individual carriers, for passive NT configurations; DMT would use FDM for upstream multiplexing (although DMT does not preclude a TDMA multiplexing strategy);
- DWMT; Discrete Wavelet Multi-Tone, a multi-carrier system using Wavelet Transforms to create and demodulate individual carriers,
 DWMT also uses FDM for upstream multiplexing, but also allows TDMA; and
- SLC; Simple Line Code, a version of four-level baseband signalling that filters the base band and restores it at the receiver, for passive NT configurations; SLC would most likely use TDMA for upstream multiplexing, although FDM is possible.

Early versions of VDSL will use frequency division multiplexing to separate downstream from upstream channels and both of them from POTS and ISDN. Echo cancellation may be required for later generation systems featuring symmetric data rates. A rather substantial distance, in frequency, will be maintained between the lowest data channel and POTS to enable very simple and cost effective POTS splitters. Normal practice would locate the downstream

10

5

15

20

10

15

20

25

channel above the upstream channel. However, the DAVIC specification reverses this order to enable premises distribution of VDSL signals over coaxial cable systems.

In a multi-carrier system, such as a DMT system, a receiver must be able to recover a sampling clock that is very accurately synchronized to a transmitter sampling clock. A known method, for achieving synchronization, uses a reserved carrier, the pilot carrier, which is transmitted with a fixed phase. The receiver sampling clock is then phase locked to the pilot carrier. Frame timing must also be recovered. In existing systems this has been achieved by using a correlation technique operating in the time domain.

With OFDM systems the frequency domain data is the Fourier transform of the received time domain OFDM frames. The time domain frames must be sampled, at the receiver, in synchronism with the transmitter, so that each received frame contains data from only a single transmitted frame. It is vital for this synchronism to be maintained in order to maintain the orthogonality of the frames.

A typical multi-carrier system, of the OFDM type, which uses a cyclic prefix, permits orthogonality to be maintained when there is a small deviation from exact frame synchronisation. Because the signalling interval includes both an entire frame and the cyclic prefix, which is a repetition of part of the frame, a frame sampled within the signalling interval will contain data from only one frame. Since the signalling interval is greater than the frame period, this gives some leeway in frame alignment.

In a multi-carrier system of the OFDM type, the control of the receiver sampling clock is critical for achieving an optimal utilization of the channel capacity. The present invention takes the data needed for this control function from the received signal in a novel manner, in particular, the present invention uses adaptive equalizer parameters for sampling clock oscillator control.

In a multi-carrier system of the OFDM type, an adaptive channel equalizer, operating in the frequency domain, is often used. The internal parameters in such

15

20

25

an equalizer contain, in addition to information about the characteristics of the channel, information which can be interpreted as the time deviation between the sampling clocks of the transmitter and the receiver. The present invention utilizes this information to control the sampling clock of the receiver in a more robust way than has previously been possible with known techniques.

Known techniques for achieving frame synchronisation do not operate entirely in the frequency domain. A technique for frame synchronisation in which only frequency domain data is employed, is described in our co-pending patent application Kgp 74/97.

The present invention is particularly suitable for use in ADSL and VDSL modems which can be used to give broadband access over copper networks with relatively stationary channels. The invention is, however, of general application and also of relevance to broadband transmission in mobile and semi-mobile systems for transmission over the radio channels.

The present invention provides an extremely robust estimation of the time deviation between the sampling clocks of the transmitter and the receiver and can handle deviations of several periods, which implies that symbol limits are also guided to the right location. The robustness is achieved by using all active carriers in the estimation.

According to a first aspect of the present invention, there is provided a receiver, for use in an OFDM type transmission system, in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, characterised in that control means are provided which control a sampling oscillator, and in that said control means include estimation means for estimating timing deviations of said sampling clock, said estimation means operating entirely on frequency domain input data.

According to a second aspect of the present invention, there is provided a receiver, for use in an OFDM type transmission system, in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part

0

15

20

25

of said frame, and in which said receiver has an adaptive equaliser having an equaliser inverse channel model, characterised in that separation means are provided for separating said equaliser inverse channel model into a first and a second part, said first part being independent of sample timing and said second part being dependent on sample timing and in that control means are provided which control a sampling oscillator in dependence on said second part.

Said control means may include estimation means for estimating timing deviations of said sampling clock, said estimation means operating entirely on frequency domain input data.

Said estimation means may estimate an approximation of a linear portion of an argument function produced by timing deviations of said sampling oscillator.

Said estimation means may be adapted to find a linear part of said argument function by taking an average slope of said argument function.

Said approximation of a linear portion of an argument function may be used as a feedback control signal for said sampling clock.

Said approximation of a linear portion of an argument function may have a slope which converges to zero as a control loop, for said sampling clock, settles.

Those parts of said equaliser inverse channel model, other than said linear portion of said argument function, may be controlled by said equaliser, which continuously adapts to variations in sampling timing.

Said equaliser and said control means may each use well defined and different portions of said equaliser inverse channel model to achieve an output frequency domain signal with zero phase deviation relative to a transmitted signal.

Said slope of said argument function, $\alpha_{\mbox{\tiny K}}$ may be estimated from the equation

15

20

$$\alpha_k = \frac{1}{N} \sum_{n} \angle \frac{X_{n,k}}{n}$$

where N is the number of active carriers and $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame.

Said slope of said argument function, $\boldsymbol{\alpha}_{k},$ may be estimated from the equation

$$\alpha_k = \frac{2}{n_2 - n_0} \left[\sum_{n=n_1+1}^{n_2} \angle X_{n,k} - \sum_{n=n_0}^{n_1} \angle X_{n,k} \right]$$

where N is the number of active carriers, $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame, indices n_0 and n_2 are the lower and upper limits respectively of the band and index n_1 divides the band into two equal parts.

On start up, frame timing may be adjusted until received frames are sampled inside a signal interval.

Means may be provided, responsive to a feed back control for said sampling oscillator, to adjust said frame timing so that frame synchronization is maintained.

According to a third aspect of the present invention, there is an OFDM type transmission system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, characterised in that said system includes a receiver as defined in any preceding paragraph.

According to a fourth aspect of the present invention, there is provided, in an OFDM type system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, a method of synchronising a receiver sampling oscillator with a transmitter sampling oscillator, characterised

10

15

30

25

by controlling said sampling oscillator with a feedback signal representing an estimation of timing deviations of said sampling clock, said estimation signal derived directly from domain input data.

According to a fifth aspect of the present invention, there is provided, an OFDM type system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, and in which said receiver has an adaptive equaliser having an equaliser inverse channel model, a method of synchronising a receiver sampling oscillator with a transmitter sampling oscillator, characterised by separating said equaliser inverse channel model into a first and a second part, said first part being independent of sample timing and said second part being dependent on sample timing and controlling a sampling oscillator in dependence on said second part.

Timing deviations of said sampling clock may be estimated entirely from frequency domain input data.

An approximation of a linear portion of an argument function produced by timing deviations of said sampling oscillator may be estimated.

A linear part of said argument function may be found by taking an average slope of said argument function.

Said approximation of a linear portion of an argument function may be used as a feedback control signal for said sampling clock.

Said approximation of a linear portion of an argument function may have a slope which converges to zero as a control loop, for said sampling clock, settles.

Those parts of said equaliser inverse channel model, other than said linear portion of said argument function, may be controlled with said equaliser, which continuously adapts to variations in sampling timing.

Said equaliser and said control means may each use well defined and

10

15

different portions of said equaliser inverse channel model to achieve an output frequency domain signal with zero phase deviation relative to a transmitted signal.

Said slope of said argument function, $\alpha_{\mathbf{k}}$, may be estimated from the equation

$$\alpha_k = \frac{1}{N} \sum_{n} \angle \frac{X_{n,k}}{n}$$

where N is the number of active carriers and $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame.

Said slope of said argument function, $\alpha_{\mathbf{k}}$ may be estimated from the equation

$$\alpha_k = \frac{2}{n_2 - n_0} \left[\sum_{n=n_1+1}^{n_2} \angle X_{n,k} - \sum_{n=n_0}^{n_1} \angle X_{n,k} \right]$$

where N is the number of active carriers, $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame, indices n_0 and n_2 are the lower and upper limits respectively of the band and index n_1 divides the band into two equal parts.

Frame timing, on start up, may be adjusted until received frames are sampled inside a signal interval.

Said frame timing may be adjusted in accordance with a feed back signal for said sampling oscillator, so that frame synchronization is maintained.

According to a sixth fifth aspect of the present invention, there is provided an ADSL modern characterised in that said modern has a receiver as defined above, or operates a method of synchronisation as defined above.

According to a sixth aspect of the present invention, there is provided a

10

15

20

25

VDSL modem characterised in that said modem has a receiver as defined above, or operates a method of synchronisation as defined above.

Embodiments of the invention will now be described, by way of example, with reference to the accompanying drawings, in which:

Figure 1 illustrates, in functional form, an equaliser and sampling control unit in which the present invention can be implemented.

Figure 2 illustrates the time domain data format of an OFDM signal used with the present invention.

The synchronisation process of the present invention is illustrated in a functional form in Figure 1. Incoming frequency domain data is passed via an equaliser to a detector/quantizer and thence to a symbol decoder. The operation of the remaining blocks shown in Figure 1, namely the equalisation parameter updating algorithm, the sampling clock control algorithm and the frame timing algorithm are explained in the following description. It is, however, worth noting at this point that:

- the equalisation parameter updating algorithm takes inputs from the raw frequency domain input data, X, the output of the equaliser, U, and the output of the detector/quantizer, Y;
- the sampling clock control algorithm receives an input from the equalisation parameter updating algorithm, as does the equaliser;
 and
- the frame timing algorithm accepts an input from the raw frequency domain input data.

The frequency-domain data comprises the received time-domain OFDM frames after Fourier transformation. The time-domain frames must be sampled in synchronism with the transmitter so that each received frame contains data from

10

15

20

25

PCT/SE98/00353 WO 98/39872 - 10 -

only one transmitted frame. This is important in order to maintain the orthogonality of the frames.

Figure 2 shows the time-domain format for the transmission of OFDM frames used with the present invention.

The signalling interval contains a cyclic prefix and a frame. The cyclic prefix is a copy of the last part of the frame. This means that a frame sampled anywhere inside the signalling interval will contain data from one transmitted frame only. A deviation from the exact frame timing will, therefore, lead to a cyclic permutation of the frame. The orthogonality will, however, be maintained.

As previously stated, the present invention relates to, among other things, a method for sampling clock oscillator control in a system of the OFDM type, which is based on adaptive equalizer information. The method of the present invention assumes that the linear part of the equalizer parameter argument vector is related to the frame timing deviation. The estimation of the frame timing deviation is performed entirely in the frequency domain and the deviation estimate is used as a feed-back control signal for the sampling clock Oscillator.

A training procedure must be used at start-up. The frame timing is adjusted until the received frames are sampled inside the signalling interval, see our co-pending patent application Kgp 74/97. The sampling clock frequency must also be adjusted so that it is sufficiently close to the transmitter clock frequency to enable the equalizer to follow changes in the timing deviation.

Frame start pulses are generated by counting sampling clock intervals. Therefore, after the initial setting of the frame start pulse timing during the training procedure, the timing of the frame start pulse will need to be modified by the feedback control of the sampling clock oscillator, in order to maintain frame synchronisation.

After the training procedure, the equalizer parameters EQ will represent the complex frequency domain inverse of the channel. If there is a deviation from the

10

15

20

25

correct timing of the time domain sampling of the frames, there will also be a linear part of the equalizer inverse channel model argument function. The adaptive equaliser constructs a model of the transmission channel and applies an inverse of this model to incoming signals - the equaliser inverse channel model.

The exact linear argument function, produced by the timing deviation, is not available, but an approximation can be estimated using the equalizer parameters. The argument function of the equalizer parameters is generally non-linear, but a linear part can be found by taking the average slope of the argument function. This slope estimate is used as a feed-back signal to control the sampling clock oscillator frequency. The slope will converge towards zero as the sampling clock control loop settles.

The rest of the equaliser inverse channel model is taken care of by the equalizer, which continuously adapts to variations in the sample timing.

The advantage of this technique is that the equalizer and the sampling control use well defined separate parts of the equaliser inverse channel model to achieve an output frequency domain signal with zero phase deviation relative to the transmitted signal.

The argument function of the equalizer parameters is the vector of arguments of the individual complex elements. The argument of a complex number is the inverse tangent of the imaginary part divided by the real part. A problem associated with this calculation is that the inverse tangent function is periodic, with a period 2π radians. In this application it is necessary to handle larger arguments than π radians, which is the range of the inverse tangent function. An assumption used here is that the difference in argument between adjacent parameters is smaller than π radians. This means that it is possible to compensate for each discontinuity caused by the inverse tangent function periodicity and thus unwrap the argument function.

The average slope, α_k of the linear part of the argument function can be calculated, as shown in equation (1), or by some other standard method, using the

10

15

20

unwrapped argument function of Xk for the kth frame

Where N is the number of active carriers and $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame.

If the lowest frequency carriers are not present in the frame, it is not possible to find the true argument function, because there will be an unknown starting value for the available part of the function. This is not a problem in the present case, since the slope can still be calculated.

Equation (2) shows an algorithm that gives the average slope of a contiguous band of active carriers. Indices n_0 and n_2 are the lower and upper limits respectively of the band. Index n_1 divides the band into two equal parts. If several separate bands are used, equation (2) is applied to each band and the average of the results is calculated.

$$\alpha_k = \frac{2}{n_2 - n_0} \left[\sum_{n=n_1+1}^{n_2} \angle X_{n,k} - \sum_{n=n_0}^{n_1} \angle X_{n,k} \right] \dots (2)$$

The algorithm, according to equation (2), gives a very simple hardware implementation for OFDM receivers.

The unique novelty in the technique of the present invention resides in the separation of the inverse channel model into two parts, one of which is sample timing dependent and the other of which is sample timing independent.

If the sample timing and the equalizer are controlled by separate techniques they might counteract each others actions, because, both the equalizer and the sample timing influence time delay. This situation could eventually lead

- 13 -

to a drift of the frame timing out of the correct interval (the cyclically permuted signal interval). This cannot happen with the technique of the present invention.

The sample timing control, provided by the present invention, is very robust against external disturbance, because every active carrier is used in the timing deviation estimation.

CLAIMS

5

10

15

0

- 1. A receiver, for use in an OFDM type transmission system, in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, characterised in that control means are provided which control a sampling oscillator, and in that said control means include estimation means for estimating timing deviations of said sampling clock, said estimation means operating entirely on frequency domain input data.
- 2. A receiver, for use in an OFDM type transmission system, in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, and in which said receiver has an adaptive equaliser having an equaliser inverse channel model, characterised in that separation means are provided for separating said equaliser inverse channel model into a first and a second part, said first part being independent of sample timing and said second part being dependent on sample timing and in that control means are provided which control a sampling oscillator in dependence on said second part.
- 3. A receiver, as claimed in claim 2, characterised in that said control means include estimation means for estimating timing deviations of said sampling clock, said estimation means operating entirely on frequency domain input data.
- 4. A receiver, as claimed in claim 3, characterised in that said estimation means estimate an approximation of a linear portion of an argument function produced by timing deviations of said sampling oscillator.
- 5. A receiver, as claimed in claim 4, characterised in that said estimation means is adapted to find a linear part of said argument function by taking an average slope of said argument function.
- 6. A receiver, as claimed in either claim 4, or claim 5, characterised in that said approximation of a linear portion of an argument function is used as a feedback control signal for said sampling clock.

.0

15

20

- 7 A receiver, as claimed in claim 6, characterised in that said approximation of a linear portion of an argument function has a slope which converges to zero as a control loop, for said sampling clock, settles.
- 8. A receiver, as claimed in claim 7, characterised in that those parts of said equaliser inverse channel model, other than said linear portion of said argument function, are controlled by said equaliser, which continuously adapts to variations in sampling timing.
- 9. A receiver, as claimed in claim 8, characterised in that said equaliser and said control means each use well defined and different portions of said equaliser inverse channel model to achieve an output frequency domain signal with zero phase deviation relative to a transmitted signal.
- 10. A receiver, as claimed in any of claims 7 to 9, characterised in that said slope of said argument function, α_k , is estimated from the equation

$$\alpha_k = \frac{1}{N} \sum_{n} \angle \frac{X_{n,k}}{n}$$

where N is the number of active carriers and $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame.

11. A receiver, as claimed in any of claims 7 to 9, characterised in that said slope of said argument function, α_k , is estimated from the equation

$$\alpha_k = \frac{2}{n_2 - n_0} \left[\sum_{n=n_1+1}^{n_2} \angle X_{n,k} - \sum_{n=n_0}^{n_1} \angle X_{n,k} \right]$$

where N is the number of active carriers, $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame, indices n_0 and n_2 are the lower and upper limits respectively of the band and index n_1 divides the band into two equal parts.

7

15

20

- 12. A receiver, as claimed in any previous claim, characterised in that, on start up, frame timing is adjusted until received frames are sampled inside a signal interval.
- 13. A receiver, as claimed in claim 12, characterised in that means are provided, responsive to a feed back control for said sampling oscillator, to adjust said frame timing so that frame synchronization is maintained.
- 14. An OFDM type transmission system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, characterised in that said system includes a receiver as claimed in any of claims 1 to 13.
- 15. In an OFDM type system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, a method of synchronising a receiver sampling oscillator with a transmitter sampling oscillator, characterised by controlling said sampling oscillator with a feedback signal representing an estimation of timing deviations of said sampling clock, said estimation signal derived directly from domain input data.
- 16. In an OFDM type system in which data is transmitted in frames, each frame having a cyclic prefix which is a repetition of part of said frame, and in which said receiver has an adaptive equaliser having an equaliser inverse channel model, a method of synchronising a receiver sampling oscillator with a transmitter sampling oscillator, characterised by separating said equaliser inverse channel model into a first and a second part, said first part being independent of sample timing and said second part being dependent on sample timing and controlling a sampling oscillator in dependence on said second part.
- 17. A method, as claimed in claim 16, characterised by estimating timing deviations of said sampling clock entirely from frequency domain input data.
- 18. A method, as claimed in claim 17, characterised by estimating an approximation of a linear portion of an argument function produced by timing

10

15

20

deviations of said sampling oscillator.

- 19. A method, as claimed in claim 18, characterised by finding a linear part of said argument function by taking an average slope of said argument function.
- 20. A method, as claimed in either claim 18, or claim 19, characterised by using said approximation of a linear portion of an argument function as a feedback control signal for said sampling clock.
- 21. A method, as claimed in claim 20, characterised by said approximation of a linear portion of an argument function having a slope which converges to zero as a control loop, for said sampling clock, settles.
- 22. A method, as claimed in claim 21, characterised by controlling those parts of said equaliser inverse channel model, other than said linear portion of said argument function, with said equaliser, which continuously adapts to variations in sampling timing.
- 23. A method, as claimed in claim 22, characterised by said equaliser and said control means each using well defined and different portions of said equaliser inverse channel model to achieve an output frequency domain signal with zero phase deviation relative to a transmitted signal.
- 24. A method, as claimed in any of claims 21 to 23, characterised by estimating said slope of said argument function, α_k , from the equation

$$\alpha_k = \frac{1}{N} \sum_{n} \angle \frac{X_{nk}}{n}$$

where N is the number of active carriers and $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame.

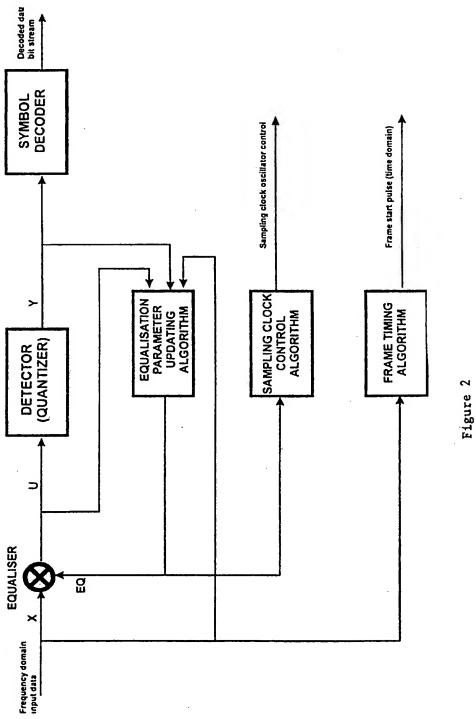
25. A method, as claimed in any of claims 21 to 23, characterised by estimating said slope of said argument function, α_k , from the equation

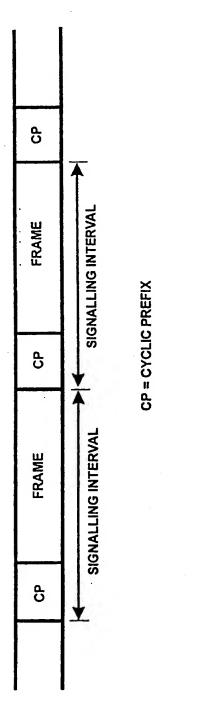
10

$$\alpha_k = \frac{2}{n_2 - n_0} \left[\sum_{n=n_1+1}^{n_2} \angle X_{n,k} - \sum_{n=n_0}^{n_1} \angle X_{n,k} \right]$$

where N is the number of active carriers, $X_{n,k}$ is the unwrapped argument function for the nth active carrier in the kth frame, indices n_0 and n_2 are the lower and upper limits respectively of the band and index n_1 divides the band into two equal parts.

- 26. A method, as claimed in any of claims 15 to 25, characterised by adjusting frame timing, on start, until received frames are sampled inside a signal interval.
- 27. A method, as claimed in claim 26, characterised by adjusting said frame timing in accordance with a feed back signal for said sampling oscillator, so that frame synchronization is maintained.
- 28. An ADSL modem characterised in that said modem has a receiver as claimed in any of claims 1 to 13, or operates a method of synchronisation as claimed in any of claims 15 to 27
- 29. A VDSL modem characterised in that said modem has a receiver as claimed in any of claims 1 to 13, or operates a method of synchronisation as claimed in any of claims 15 to 27.





igure 2